

KITZ

Special Alloy Steel (Cast) Valves



KITZ CORPORATION

Approach to Corrosive Environment

KITZ High Corrosion Resistant Material Special Alloy Steel



Customers with corrosion concern might be looking for following material.

Higher corrosion resistant material than current valve material at lower cost.

Valve material with longer valve replacement period to reduce maintenance cost.

KITZ can supply customers with high corrosion resistant material to fit their corrosive environments by material selection based on own corrosion test data from wide range of lineups from stainless steel casting to high nickel alloy steel casting.

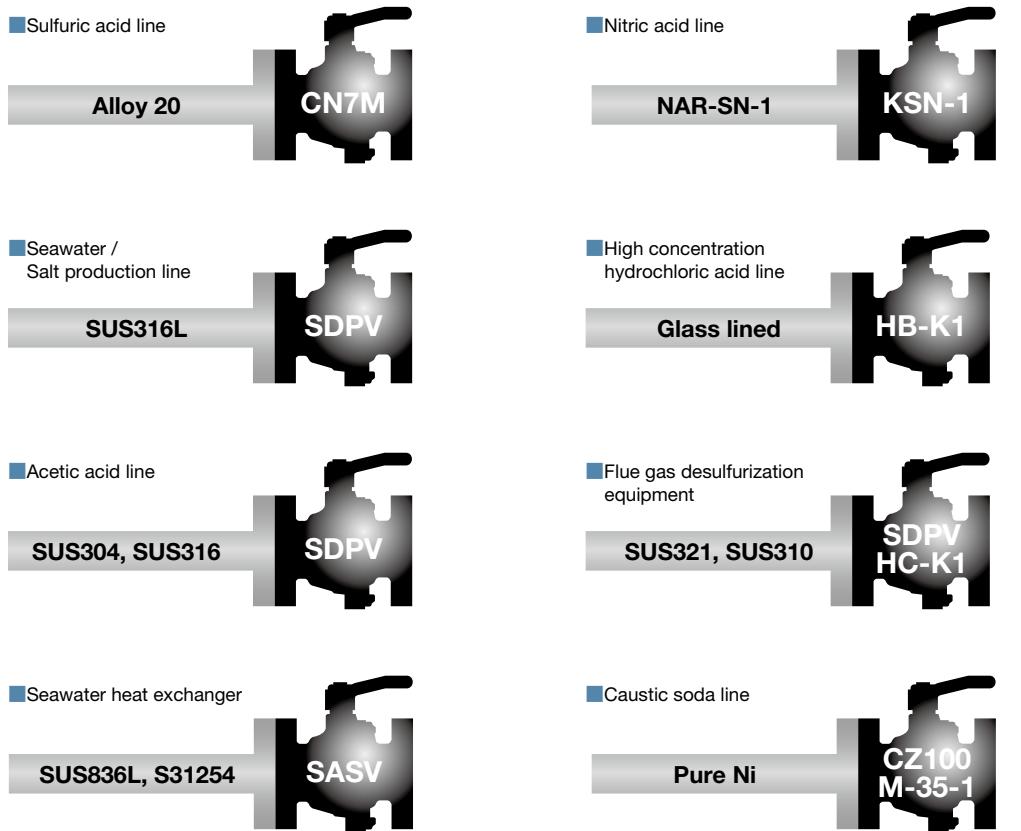
KITZ can meet customers' requirements with producing even 1piece of high nickel alloy valve at own casting facilities.

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1. KITZ Selects Proper Valve Material from Piping Material and Operating Environment.

■ Valve Material Selection Example



Point in selecting valve material

- Valves have more gaps than pipes.
- Valves have higher crevice corrosion risk than pipes.

It is required to select higher corrosion resistant valves than pipes depending on operating environment.

2. Is Cost Too High with the Valve Material Selection ?

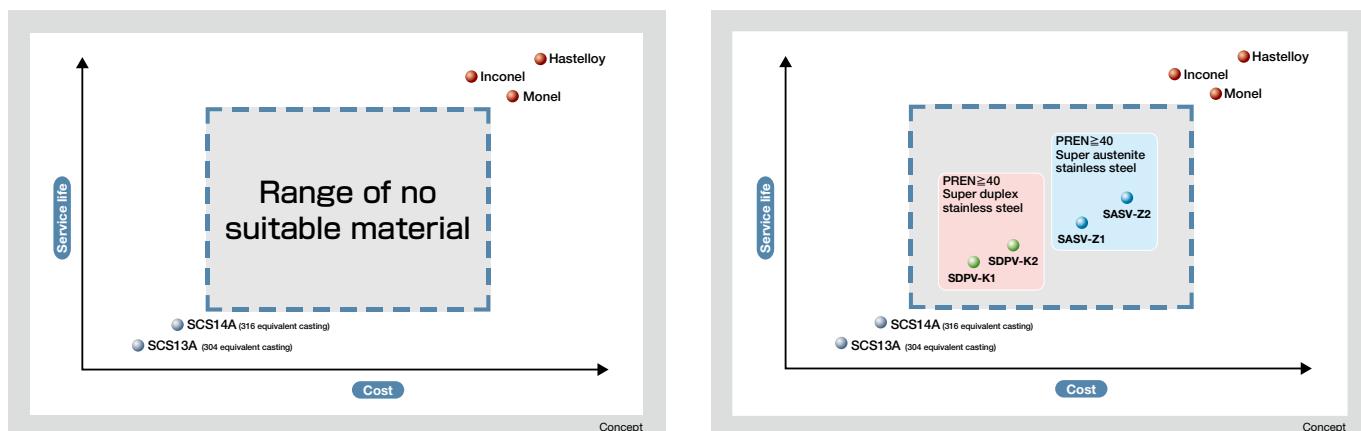
When you select valve material until now ...?

You had to select much higher cost material than SCS13A or SCS14A.

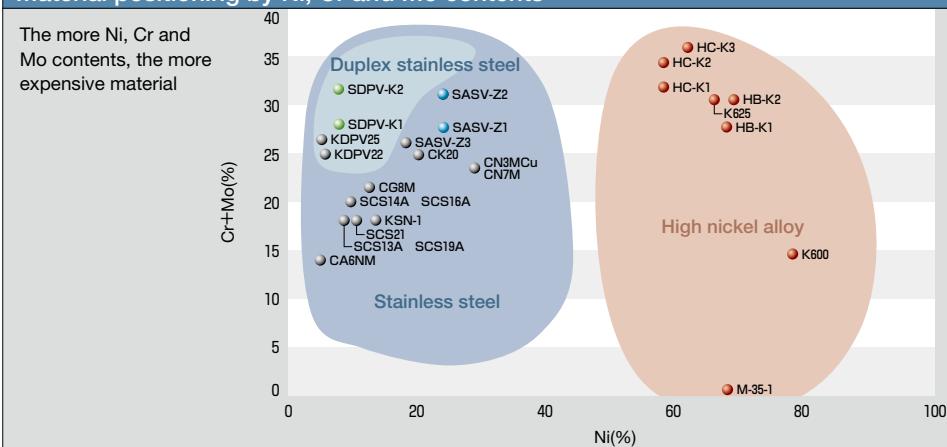
KITZ has wide variety of material to be selected.

KITZ collected wide variety of valve material.

You can select material with high corrosion resistance at reasonable cost.

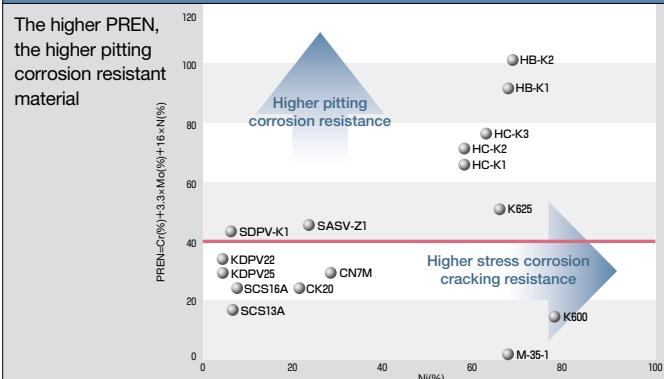


Material positioning by Ni, Cr and Mo contents



3. Material Positioning by Characteristics

Positioning by pitting corrosion resistance

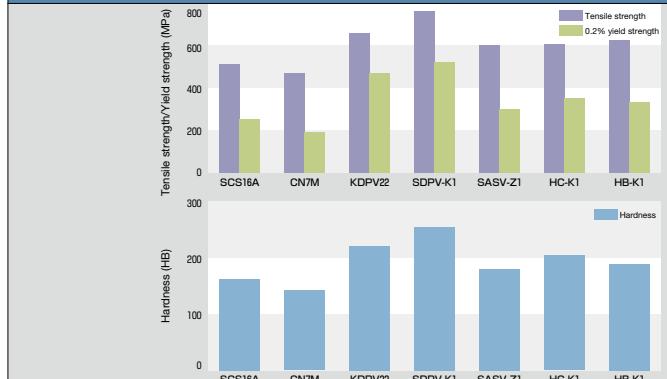


PREN : Pitting Resistance Equivalent Number

PREN = Cr(%) + 3.3xMo(%) + 16xNi(%) PREN is digitized pitting corrosion resistance.

● The higher PREN, the higher pitting corrosion resistant material. ● Material with PREN≥40 has "Super" as capital letter.

Mechanical properties of stainless steel and high nickel alloy casting



4. KITZ Valve Advantages

1 Quality

Integrated production from casting (material) with own casting facilities.

2 Variety

Wide range of material lineups from stainless steel to high nickel alloy casting.

3 Flexibility

Flexibility to produce even 1 piece of special stainless steel and high nickel alloy valve.

4 Economy

The most suitable material valve can be offered for specific operating environment based on our internal corrosion test data.

5. Production Location

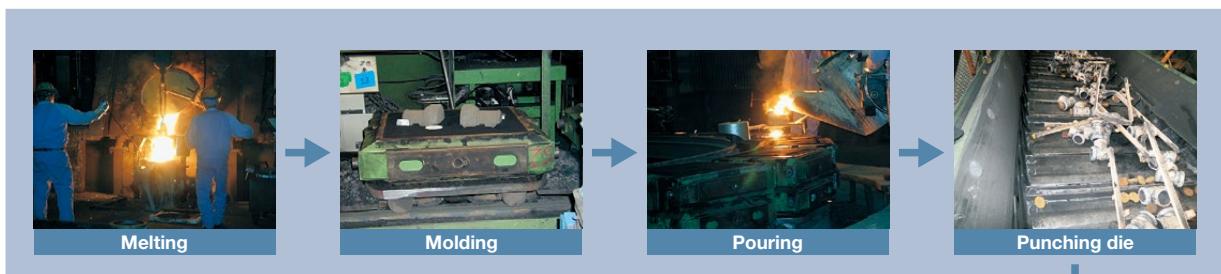
Nagasaki Plant

Manufacturing plant exclusively for stainless steel to high nickel alloy casting valves.



6. Production Engineering

1 Melting/Casting Process



2 Point of Production Engineering

Casting plan

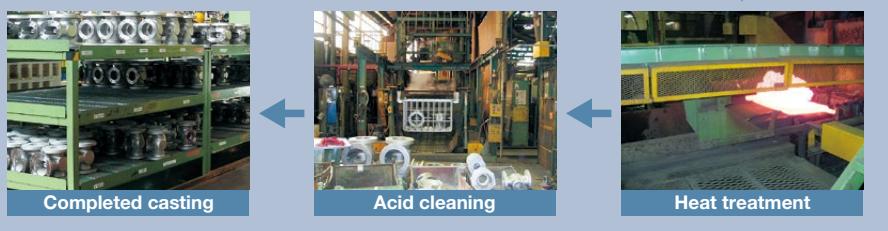
Solidification simulation

Melting

SRP furnace (KITZ original)
Stainless Refining Process

Heat treatment

EMF (Furnace exclusive for special
stainless steel and high nickel alloy casting)
Exotic Material Furnace



					(2) PREN	Mechanical properties			Characteristics	Application	Equivalent (Trademark)	
Cu	Fe	V	W	N		Tensile strength (N/mm²)	Yield strength (N/mm²)	Elongation (%)				
-	Balance	-	-	-	-	480~	205~	33~	High corrosion resistance to nitric acid, phosphoric acid and organic acid. Less corrosion resistance to sulfuric acid.	For corrosion resistance required process at various plants	-	
-	Balance	-	-	-	-	485~	205~	35~				
-	Balance	-	-	-	-	480~	205~	33~	Upgraded intergranular corrosion resistance type of SCS13A.	For intergranular corrosion resistance process of SCS13A	-	
-	Balance	-	-	-	-	485~	205~	35~				
-	Balance	-	-	-	-	480~	205~	33~	High corrosion resistance to environments other than hydrochloric acid, hydrofluoric acid, high temperature and high concentration of sulfuric acid and phosphoric acid.	For severer environments than SCS13A process	-	
-	Balance	-	-	-	-	485~	205~	30~				
-	Balance	-	-	-	-	480~	205~	33~	Upgraded intergranular corrosion resistance type of SCS14A.	For intergranular corrosion resistance process of SCS14A	-	
-	Balance	-	-	-	-	485~	205~	30~				
-	Balance	(Nb=10×C%~1.35)		-	-	480~	205~	28~	Higher intergranular corrosion resistance than SCS13A with stabilized carbide by adding Nb.	For hydrogenation desulfurizing equipment	-	
-	Balance	(Nb= 8×C%~1.00)		-	-	485~	205~	30~				
-	Balance	-	-	-	-	515~	240~	25~	Upgraded pitting corrosion resistance and crevice corrosion resistance type of SCS14A.	For acetic acid process	-	
-	Balance	-	-	-	-	515~	240~	25~	Upgraded intergranular corrosion resistance type of CG8M.	For intergranular corrosion resistance process of CG8M	-	
						480~	230~	10~	High corrosion resistance to total concentration of nitric acid and fuming nitric acid environments.	For nitric acid process	NAR®-SN-1	
3.00~4.00	Balance	-	-	-	-	390~	165~	30~	High corrosion resistance to all concentration of sulfuric acid below 60 degree C and heated solution of dilute oxide.	For sulfuric acid (the most common)	-	
3.0~4.0	Balance	-	-	-	-	425~	170~	35~				
3.0~3.5	Balance	-	-	-	-	425~	170~	35~	Higher sulfuric acid corrosion resistance than CN7M with 95% or more of refined material such as AOD and VOD.	Longer life type of CN7M	-	
-	Balance	-	-	-	-	450~	195~	28~	Higher Cr and Ni than SCS13A and used in environments such as sulfuric acid solution and nitric acid at room temperature.	For low concentration of alkali and nitric acid process	-	
-	Balance	-	-	-	-	450~	195~	30~				
~0.75	Balance	-	-	0.18~0.26	45~	550~	260~	35~	The highest acid resistance and alkali resistance among general austenitic stainless steel. High pitting corrosion resistance and crevice corrosion resistance to chloride solution such as seawater.	Higher grade than SDPV (less hardness)	-	
						50~	550~	260~	20~	Higher pitting factor than SASV-Z1 with high Cr and suitable for seawater resistant environments at high temperature.	Higher grade than SDPV (the highest grade SASV)	-
0.50~1.00	Balance	-	-	0.18~0.24	40~	550~	260~	35~	Steel corresponding to AVESTA 254SMO which is commonly used in the world.	Higher grade than SDPV (less hardness)	254SMO®	
~1.00	Balance	-	-	0.10~0.30	-	620~	415~	25~	Higher SCC resistance and pitting corrosion resistance in intermediate concentration of chloride environments. Higher general corrosion resistance to environments such as dilute sulfuric acid and phosphoric acid.	For seawater environments and oil well (mild environments such as North Sea oil well)	SAF 2205®	
2.7~3.3	Balance	-	-	0.10~0.25	-	690~	485~	16~	Suitable for nitric acid in oxidizing environments and sulfuric acid in reducing environments with higher addition of Cr and Cu than KDPV22.	For seawater environments and oil well sulfuric acid process	-	
-	Balance	-	-	0.08~0.30	40~	620~	390~	15~	Higher SCC resistance than austenitic stainless steel and higher weldability than ferritic stainless steel. High mechanical strength and higher acid resistance, pitting corrosion resistance and crevice corrosion resistance than SCS16A.	For seawater environments, oil well and seawater desalination process (domestic)	-	
					45~	620~	390~	15~	KITZ originally developed, the highest pitting factor among SDPV series and suitable for high temperature seawater environments. Suitable for methionine process in oxidizing environments with high Cr.	For seawater desalination process (the highest grade duplex stainless steel)	-	
0.5~1.0	Balance	-	0.5~1.0	0.20~0.30	40~	700~	450~	25~	Used for overseas seawater desalination process.	For seawater environments, oil well and seawater desalination process (overseas)	-	
-	Balance	-	-	0.10~0.30	40~	690~	515~	18~	Higher PREN than SDPV-K1 and K3 with high mechanical strength.	For seawater environments, oil well and seawater desalination process (overseas) (higher grade than SDPV-K3)	SAF 2507®	
26.0~33.0	~3.5	(Nb= ~0.5)		-	450~	170~	25~	High corrosion resistance in reducing environments without local corrosion and insensitive to SCC by Cl ⁻ .	For intermediate concentration of alkali and pure oxygen	Monel®400		
-	~11.0	-	-	-	-	485~	195~	30~	High oxidation resistance at high temperature to oxidizing acid such as nitric acid. High SCC resistance by Cl ⁻ and high corrosion resistance to high pure water and alkali.	For high temperature process and intermediate concentration of alkali	Inconel®600	
-	4.0~6.0	0.20~0.60	-	-	-	525~	275~	6~	Corrosion resistant to hydrochloric acid at all concentrations to boiling point. Corrosion resistant to reducing acid such as sulfuric acid up to 60%, phosphoric acid and cupric chloride. High temperature resistant but not suitable for strong oxidizing environments such as nitric acid.	For high concentration of hydrochloric acid process (not suitable for nitric acid)	Hastelloy®B	
-	~3.0	-	-	-	-	525~	275~	20~	High corrosion resistance at welded part with high weldability.	Higher grade type of HB	Hastelloy®B2	
-	4.5~7.5	0.20~0.40	3.75~5.25	-	-	495~	275~	4~	High corrosion resistance in oxidizing environments such as wet chlorine gas and chlorine dioxide. High corrosion resistance to organic acid and salt such as acetic acid and seawater.	For seawater environments, oil well (high concentration of H ₂ S) and flue gas desulfurization process (not suitable for nitric acid)	Hastelloy®C276	
-	2.0~6.0	~0.35	2.5~3.5	-	-	550~	310~	30~	High corrosion resistance in oxidizing environments by high Cr and low Mo with improved mechanical properties.	For mixed acid (sulfuric acid and nitric acid) Improved type of HC-K1	Hastelloy®C22	
-	~3.00	-	-	-	-	495~	275~	25~	High corrosion resistance in oxidizing environments and reducing environments by high Cr and low Mo. Commonly used overseas.	Intermediate material between HC-K1 and HC-K2	-	
-	~2.0	-	~1.0	-	-	495~	275~	20~	Equivalent material to HC-K1 and commonly used overseas.	Inexpensive type of HC-K1	Hastelloy®C4	
-	~5.0	(Nb=3.15~4.50)		-	485~	275~	25~	High corrosion resistance in oxidizing environments at high temperature. High corrosion resistance in erosive environments.	For high temperature process, seawater environments and oil well (high concentration of H ₂ S)	Inconel®625		
1.5~3.5	Balance	(Nb=0.60~1.20)		-	520~	240~	20~	High SCC resistance and crevice corrosion resistance to sulfuric acid and phosphoric acid.	For high temperature process, seawater environments and oil well	Incoloy®825		
~1.25	~3.00	-	-	-	-	345~	125~	10~	High corrosion resistance to alkali hydroxide solution and fused alkali such as sodium hydroxide and potassium hydroxide.	For high concentration of alkali (for caustic soda)	Nickel 200®	

8. Corrosion Resistance Evaluation of Material under Corrosive Environment

These evaluations are average values of laboratory test data and do not guarantee any maximum or minimum values and corrosion resistance in the actual environment.

Ferric Chloride Crevice Corrosion Test (12.7% FeCl₃:6H₂O:Temperature30°C)

Corrosion evaluation	SCS14A	SCS16A	CN7M	SASV-Z1	SDPV-K1	SDPV-K2	HC-K1
Corrosion rate	▲	▲	▲	●	●	●	●
Number of crevice corrosion	40/40	40/40	39/40	0/40	14/40	2/40	0/40

Hydrochloric Acid

Concentration	Temperature	SCS13A	SCS16A	CN7M	SASV-Z1	SDPV-K1	HB-K1	HC-K1
5%	Boiling	▲	—	—	▲	●	—	—
10%	Boiling	—	—	—	▲	—	●	●
20%	40	—	●	●	●	●	●	●
	80°C	▲	▲	▲	●	●	●	●
40%	40°C	—	●	●	●	●	●	●
	80°C	▲	▲	●	▲	▲	●	●
60%	40°C	—	▲	●	●	●	●	●
	60°C	▲	—	●	●	▲	—	—
80%	40°C	▲	▲	●	●	▲	●	●
	80°C	—	▲	●	●	▲	●	●
98%	40°C	●	●	●	●	●	—	—
	80°C	▲	▲	▲	▲	▲	●	●

Caustic Soda

Concentration	Temperature	M-35-1
20%	Boiling	●
40%	100°C	●
	Boiling	●
60%	100°C	●
	Boiling	●
80%	100°C	●
	150°C	●
	Boiling	●

Chlorine Dioxide

Concentration	Temperature	SCS14A	SASV-Z1	SDPV-K1	HB-K1	HC-K1	T1
2000ppm	95°C	●	●	●	▲	●	●

General Corrosion Test Example

KITZ material name	SCS16A	SDPV-K1	SASV-Z1	CN7M	HC-K1	HB-K1	
Standards	JIS G5121 SCS 16A	JIS G5121 SCS 10	—	JIS G5121 SCS 23	JIS H5701 NMCrC	JIS H5701 NMC	
	ASTM A351 CF3M	—	ASTM A351 CN3MN	ASTM A351 CN7M	ASTM A494 CW-12MW	ASTM A494 N-12MV	
	UNS J92800	—	—	UNS J95150	UNS N30002	UNS N30012	
Test condition	A H ₂ SO ₄ :40%, 80°C						
	B H ₂ SO ₄ :60%, 80°C						
Test condition	Test solution	Concentration	Temperature	Permeation period			
A	H ₂ SO ₄	40%	80°C	24hr			
		60%					

Memo

10. KITZ Special Alloy Steel Valve Range of Use

■ Pressure/Temperature Rating (P/T Rating)

The valve material strength changes by the temperature, which determines maximum allowable pressure of the valve.

Pressure/temperature rating shows relationship between valve temperature and maximum allowable pressure to be used.

The relationship is established in JIS B2220 (Steel pipe flanges) and JIS B2071 (Steel flanged valves) by material and structure.

The rating is defined in ANSI/ASME B16.34 (Valves-Flanged, Threaded and Welding End) as PRESSURE-TEMPERATURE RATING in USA.

It is also defined in JPI 7S-65 as steel valve pressure-temperature standard.

These standards categorize many materials to be used by their properties and define maximum allowable pressure from ambient to high temperature.

It is required to select valves which meet operating conditions from the pressure/temperature rating with economical efficiency.

10-1. Pressure/Temperature Rating (JIS 10K/20K)

Type	Size			10K							20K										
	Material			Operating temperature																	
	KITZ	JIS	ASTM	°C	-120	220	260	300	350	400	425	-120	220	260	300	316	325	350	400	425	
Austenitic stainless steel casting																					
Iron-based alloy	SCS21	CB	SCS21	A351 Gr.CF8C	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	CG8M	CG	—	A351 Gr.CG8M	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	CG3M	GM	—	A351 Gr.CG3M	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	KSN-1	SN	—	—	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	CN7M	CN	SCS23	A351 Gr.CN7M	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.8	—	—
	CN3MCu	3M	SCS23 equiv.	A990 Gr.CN3MCu	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.8	—	—
	CK20	CK	SCS18	A351 CK20	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
Super austenitic/duplex/super duplex stainless steel casting																					
Iron-based alloy	SASV-Z1	SA	—	A351 Gr.CN3MN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	KDPV22	4A	—	A995 Gr.4A, CD3MN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	—	—
	SASV-Z2	SA	—	—	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	—	—
	SDPV-K1	SD	SCS10 equiv.	—	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9	2.8	—	—	—	—
	SDPV-K2	SD	SCS10 mod.	—	A995 Gr.5A, CE3MN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9	2.8	—	—	—
Nickel-based alloy	SASV-Z3	SA	—	A351 Gr.CK3MCuN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	—
	KDPV 25	1B	—	A995 Gr.1B, CD4MCuN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	—
	SDPV-K3	SD	—	A995 Gr.6A, CD3MWCuN	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	—
Ni-Cu/Ni-Cr/Ni-Mo/Ni-Cr-Mo alloy casting																					
Nickel-based alloy	M-35-1	NC	NCuC	A494 Gr.M35-1	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	K600	CY	NCrFC	A494 Gr.CY40	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	K625	CW	—	A494 Gr.CW6MC	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	HB-K1	HB	NMCN	A494 Gr.N12MV	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	HC-K1	HC	MCrC	A494 Gr.CW12MW	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	HB-K2	HB	—	A494 Gr.N7M	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	2.0
	HC-K3	HC	—	A494 Gr.CW6M	MPa	1.4	1.2		1.0	—	—	—	3.4	3.1		2.9			2.6	2.3	—
Ni casting																					
Ni casting					°C	-29 ~38	93	149	204	260	300	316	-29 ~38	93	149	204	260	316			
	CZ-100	CZ	—	A494 Gr.CZ100	MPa	1.13	1.10	1.03	1.03	0.99	0.97	—	2.99	2.89	2.75	2.75	2.62	2.55			

Notes

1. The above chart does not indicate JIS/ASME standards latest values.

2. The range of use may be limited by valve structures and specifications.

It is required to consider operating temperature of packing and gasket and seat rating of ball seat.

	427	450	455	475	482	500	538	550	575	600	625	650	675	700	725	750	775	800	816		Applicable standards										
	800	842	850	887	900	932	950	1000	1022	1050	1067	1100	1112	1150	1157	1200	1202	1247	1250	1292	1300	1337	1350	1382	1400	1427	1450	1472	1500		
16.73	167.3	158.2	140.9	126	124.9	119.7	99.0	69.3	51.5	39.8	28.1	19.9	15.5	12.3	10.1	9.5															
2,435		15.82	2,245	14.09	13	12.49	11.97	9.90	6.93	5.15	3.98	2.81	1.99	1.55	1.23	1.01	0.95														
144.2	144.2	143.4	140.9	126.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-2.11A		
14.42	14.42	14.34	14.05	13.00	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-2.2A		
2,110		2,090	2,075	1,930	1,820	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-2.2A		
144.2	144.0	14.00	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-2.1A conformity)		
2,110		2,090	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-3.17A		
140	14	2,030	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-2.8A conformity)		
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-2.8A conformity)		
138.0	138.0	133.7	129.2	117	114.7	108.3	97.1	84.1	70.4	57.6	43.8	31.7	22.3	15.7	11.4	9.5													ASME B16.34 Table 2-2.12A		
2,050		1,990	1,920	1,850	1,690	1,630	1,455	1,250	1,030	825	600	410	275	190	135	—	—	—	—	—	—	—	—	—	—	—	—	—	—		
2,160	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-3.12A		
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-2.8A conformity)		
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-2.8A conformity)		
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-2.8A		
134.5	134.5	103.8	10.38	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-3.4A		
2,290		1,885	1,370	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—		
136.1	136.1	133.9	131.6	126.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-3.15A conformity)		
2,005		1,970	1,930	1,895	1,895	1,820	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-3.15A		
136.1	136.1	133.9	131.6	126.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	ASME B16.34 Table 2-3.15A		
2,005		1,970	1,930	1,895	1,895	1,820	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-3.15A conformity)		
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-3.15A conformity)		
169.0	169.0	158.2	140.9	126.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	KITZ original ^{®3} (ASME B16.34 Table 2-3.8A conformity)		
2,540		2,435	2,245	1,930	1,820	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—		

Reference (Basic Terms)

Item	Description
Ferrite content calculation method and effect	<ul style="list-style-type: none"> 1. ASTM A800 (applicable only to SUS304, SUS316 and their equivalent) 2. Q Factor (applicable only to duplex stainless steel) 3. Increased strength at room temperature and improved weldability (toughness is degraded when too much [impact value at room temperature : 250J at 20%, 235J at 60%, 185J at 70% and 70J at 80%]) (extremely less strength at high temperature)
475°C embrittlement	<ul style="list-style-type: none"> 1. Embrittlement when maintained at 300 to 500°C and no microstructure change. (outstanding at 450 to 530°C at electron microscope level) 2. Outstanding with high Cr. (a few minutes with 28Cr) 3. Solved when heated at \approx 600°C.
σ phase embrittlement	<ul style="list-style-type: none"> 1. σ phase is separated when maintained at 800 to 1000°C. Outstanding at 850 to 950°C. Detected at x100 when KOH electrolytic etched. Composition is Fe+Ni \approx 50%, Cr+Mo \approx 50%. 2. Outstanding with high Cr. (1 minute with 28Cr) Separated for very short period with fine grain and highly distorted, which requires caution. 3. 5% separation makes toughness at room temperature zero, which requires caution. 4. Solved when heated at 1120°C and up (high temperature is required for high Cr)
Intermetallic compound	<ul style="list-style-type: none"> 1. Separation of higher concentration composition than base metal such as μ phase and P phase for HC material. (42Mo-10W-11Cr-33Ni for base metal 15Cr-16Mo-4W) 2. Laves phase (Fe₂Nb) and γ' phase Ni₃Al are common. 3. Solved with proper soaking.
Deformation induced martensite	<ul style="list-style-type: none"> 1. SUS304 is metastable austenitic stainless steel rather than complete austenitic stainless steel. Therefore it is changed into its original stable martensitic steel when distorted at processing or maintained at low temperature. (Md30 : Temperature that 50% martensite is generated with 30% process distortion at) 2. Ms point : Martensite transformation start temperature. 3. Mf point : Martensite transformation finish temperature.
Weldability	<ul style="list-style-type: none"> 1. Appropriate ferrite content : Ferrite improves weldability since it dissolves [S], which deteriorates weldability, and decreases segregation to grain boundary. (appropriate range is 4 to 15% considering grain refining effect)

Memo

CAUTION

Pressure-temperature ratings and other performance data published in this catalog have been developed from our design calculation, in-house testing, field reports provided by our customers, and/or published official standards or specifications. They are good only to cover typical applications as a general guideline to users of KITZ products introduced in this catalog.

For any specific application, users are kindly requested to contact KITZ Corporation for technical advice, or to carry out their own study and evaluation for proving the suitability of these products to such an application. Failure to follow this request could result in property damage and / or personal injury, for which we shall not be liable.

While this catalog has been compiled with the utmost care, we assume no responsibility for errors, impropriety, or inadequacy. Any information provided in this catalog is subject to from-time-to-time change without notice for error rectification, product discontinuation, design modification, new product introduction, or any other cause that KITZ Corporation considers necessary. This edition cancels all previous issues.

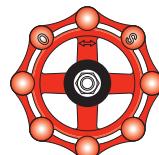
Read the instruction manual carefully before use.

NOTICE

If any products designated as strategic material in the Foreign Exchange and Foreign Trade Law, Cabinet Order Concerning Control of Export Trade, Cabinet order Concerning Control of Foreign Exchange, and other related laws and ordinances ("Foreign Exchange Laws") are exported to any foreign country or countries, an export license issued by the Japanese Government will be required under the Foreign Exchange Laws.

Further, there may be cases where an export license issued by the government of the United States or other country will be required under the applicable export-related laws and ordinances in such relevant countries.

The contract shall become effective subject to the fact that a relevant export license is obtained from the Japanese Government.



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